

SCM1209A 9-24V Transformer Driver for Isolated Power Supplies

Features

- Push-Pull Driver for Small Transformers
- Two built-in power MOSFET and Simple application circuit
- Limited MOSFET current at start-up
- Output short circuit protection and over temperature protection with self-recovery function
- Under voltage protection
- Meet 9~24V input 3.3-24V output 1-3W applications
- 220uF-4000uF capacitive load

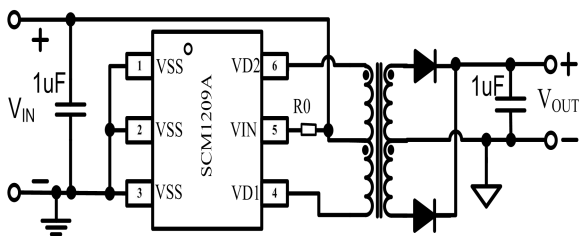
Application

- Isolated Interface Power Supply for CAN, RS-485, RS-232
- DC-DC Isolation Converter
- Distributed generation resources

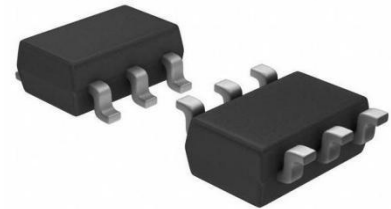
Function Description

The SCM1209A is a raw side push-pull controller designed specifically for small form factor isolated power supplies in isolated interface applications. Simply match a simple peripheral circuit to achieve 9-24V input, 3.3-24V output, power 1-3W isolated power supply. The chip consists of an oscillator, two drivers and two power switching tubes, each driver controlling the current flow of one winding on the primary side. Each way includes a power NMOS tube, and the two alternating drives achieve the push pull control of the original side. The internal logic ensures the first open and then close operation between the two power tube switches. In addition, the SCM1209A also integrates a variety of protection functions such as undervoltage and overtemperature to ensure the reliability of the converter. Its soft starting feature can prevent the large current impact during the machine starting process; The design of short circuit timing and current limiting drive decouple the capacitive load capacity from the short circuit protection capacity. Adjust the short-circuit protection threshold according to the input voltage and temperature, so that the consistency of the capacitive load and short-circuit protection is good, and is not affected by the input and temperature.

Typical Application Circuit

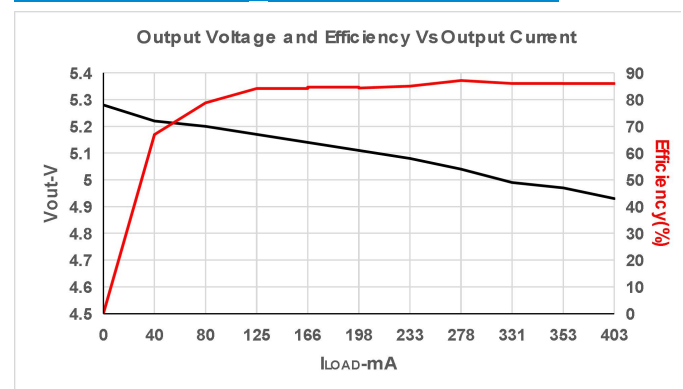


Packaging



Optional Packaging of Product: TSOT-23-6, please refer to "Ordering Information" for details of silk screen.

Function Curves

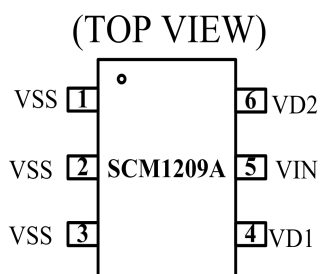


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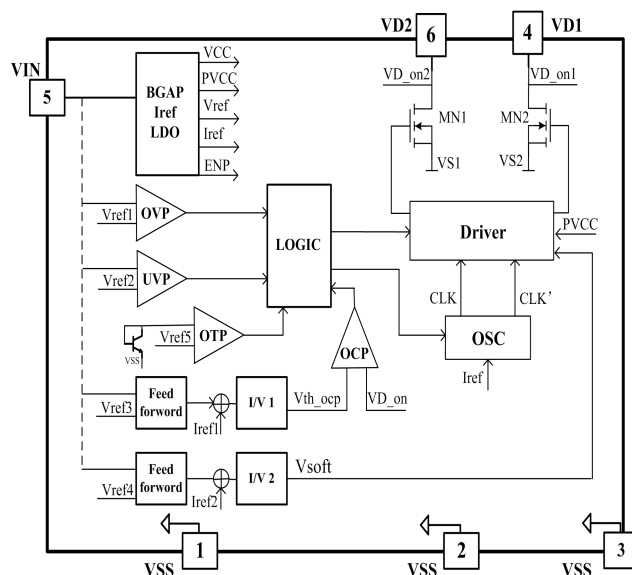
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Pin Packaging



Inter Block Diagram



Pin Description

Pin Number	Name	I/O	Description
2	VSS	I	Device ground. Connect this pin to board ground.
1,3	VSS	I	Pin1 and Pin3 is connected to the source of the power MOSFETs.
	VSS	I	
4	VD1	I	Open Drain output of the first power MOSFET. Connect this pin to one end of the transformer primary side.
6	VD2	I	Open Drain output of the second power MOSFET. Connect this pin to the other end of the transformer primary side.
5	VIN	P	Supply voltage input.

Absolute Maximum Ratings

General test conditions: Free-air, normal operating temperature range (unless otherwise specified).

Parameters		Min	Max	Unit
Input Voltage	V_{VIN}	-0.4	72	V
Drain Voltage of MOSFET	V_{VD1}/V_{VD2}	-0.7	72	V
Operation Junction Temperature Range	T_J	-40	150	°C
Storage Temperature	T_{STG}	-55	150	
Soldering Temperature (Allowable reflow soldering temperature of chip within 10 seconds)			260	
Rated Value of ESD	HBM		2500	V
	CDM		1000	

Note: if the value exceeds the stress value listed in the table's "maximum value", it may cause permanent damage to the components. If the product operates in the maximum rated condition for a long time, the reliability of the components may be affected. All voltage values take GND as basis reference. The current refers to the current between positive input and negative output of the specified terminal.

Recommended Operating Conditions

Unless otherwise specified, the following parameters are measured in the conditions of $V_{VIN}=24V$.

Parameters		Min	Max	Unit
Input Voltage	V_{VIN}	8	30	V
Drain Voltage of MOSFET	V_{VD1}/V_{VD2}	0	60	V
Output Switching Current of Primary Winding	I_{D1}, I_{D2}	300	600	mA
VD1,VD2 average switching frequency	F_{SW}	238	282	KHz
Operation Junction Temperature	T_J	-40	125	°C

Electrical Characteristics

Unless otherwise specified, $V_{VIN}=24V$ and the environment temperature is 25°C.

Symbol	Corresponding Parameters	Test Conditions	Min	Typ	Max	Unit
Voltage Supply (VIN Pin)						
V_{VIN}			8.1		30	V
I_{RUN}	Operating Current of Chip	No connection to VD1 and VD2		0.85	1	mA
I_{START}	I_{VIN} when V_{VIN} is in under-voltage lockout	$V_{VIN}=3V$			350	uA
V_{VIN_ON}	Start-up Voltage	V_{VIN} voltage increasing		7.5		V
V_{VIN_OFF}	Voltage when V_{IN} is in under-voltage lockout	V_{VIN} voltage decreasing		6.7		V
V_{VIN_OVP}	Voltage when V_{VIN} is In over voltage protection	V_{VIN} voltage increasing		35.2		V
V_{OVP_OFF}	Voltage when V_{VIN} is In over voltage lockout	V_{VIN} voltage decreasing		28.8		V
T_{OTP}	Temperature of Over-temperature Protection	Temperature increasing		156		°C
T_{OTPH}	Return Difference of Over-temperature Protection	Temperature decreasing		25		°C
Drain Output of MOSFET (VD1/VD2 Pin)						
B_{VDSS}	Breakdown Voltage of MOS Transistor	$V_{GATE}=0V, I_{DS}=100uA$	72	80		V
R_{DS_ON}	On Resistance	$V_{VIN}=24V, T_J=25^{\circ}C, I_{DS}=0.5A$		1		Ω
		$V_{VIN}=24V, T_J=100^{\circ}C, I_{DS}=0.5A$		1.5		
I_{SOFT}	Current of Soft Start	$V_{VIN}=9V, V_{VD1}=V_{VD2}=5V$	500		650	mA
		$V_{VIN}=24V, V_{VD1}=V_{VD2}=5V$	200		300	
Internal Time Parameters						
F_{OSC}	Operating Frequency	No connection to VD1 and VD2		260		kHz
T_{DEAD}	Maximum dead time	VD1,VD2 is in series with 100Ω/1W power resistance		150		ns
T_{D_OSP}	Delay Time of Short Circuit Protection	At a Fixed Operating Frequency(f_{sw}) $T=1/f_{sw}$		$2^{12}+2^{13}$		T
T_{SLEEP}	Sleep Time of Short Circuit Protection	At a Fixed Operating Frequency(f_{sw}) $T=1/f_{sw}$		2^{18}		T

Typical Performance Curves

Unless otherwise specified, the following typical characteristic curves are obtained in the conditions of $V_{IN}=24V$ and $T=25^{\circ}C$. Typical performance curves are obtained by testing the test circuit shown in Figure 5 and Figure 7.

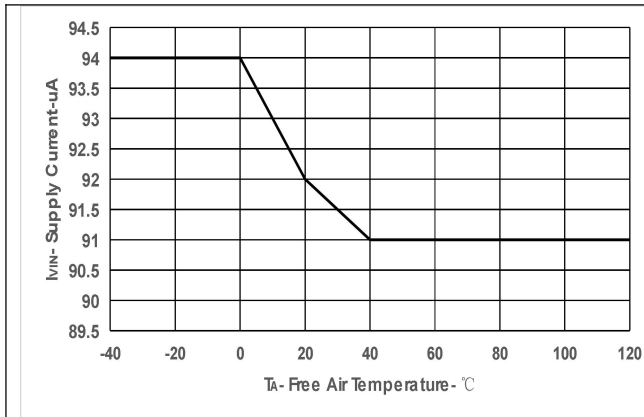


Figure 1 Average Supply Current of VIN VS Free Air Temperature

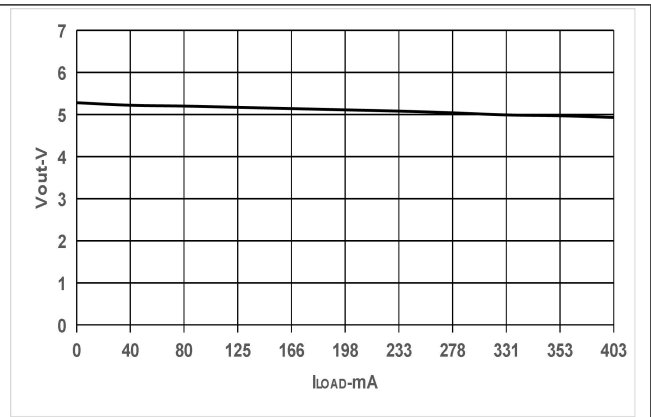


Figure 2 Output Voltage VS Load Current

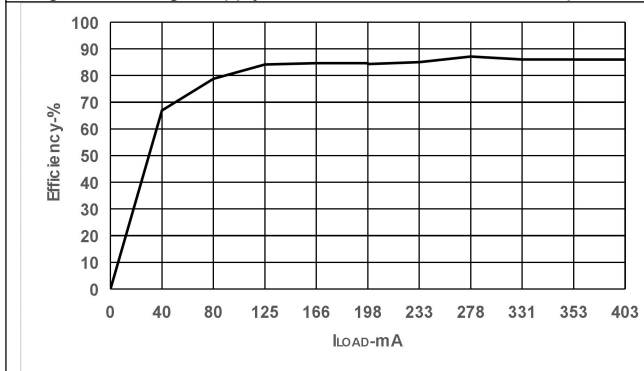


Figure 3 Efficiency VS Load Current

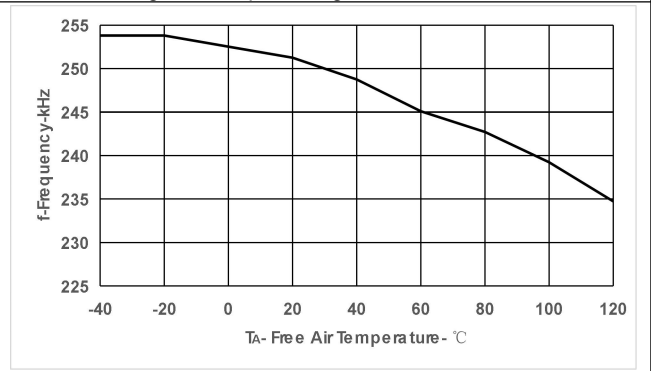


Figure 4 MOSFET Switching Frequency VS Environment Temperature

Parameter Measurement Information

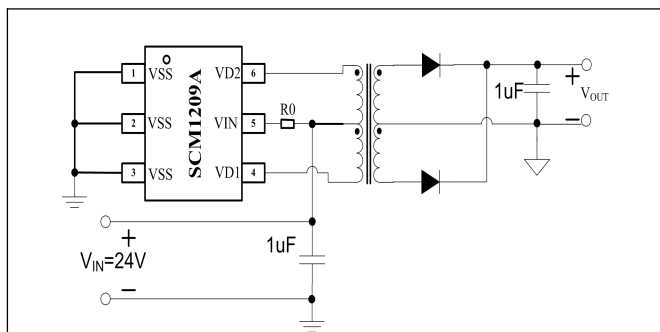


Figure 5 Schematic Diagram of Test Circuit for Function Curve

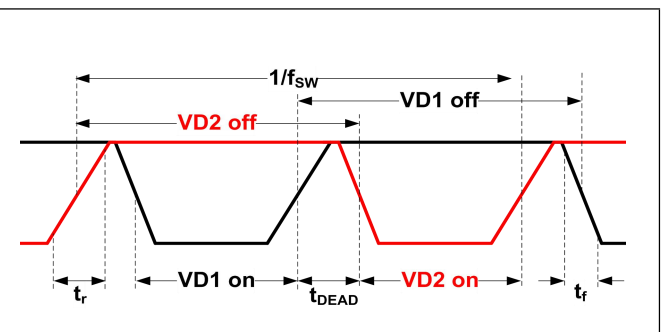


Figure 6 Circuit Sequence Diagram

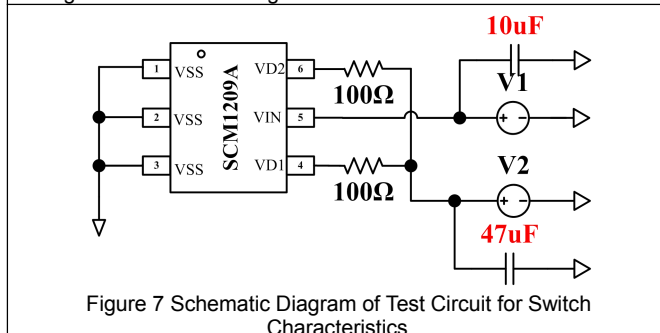
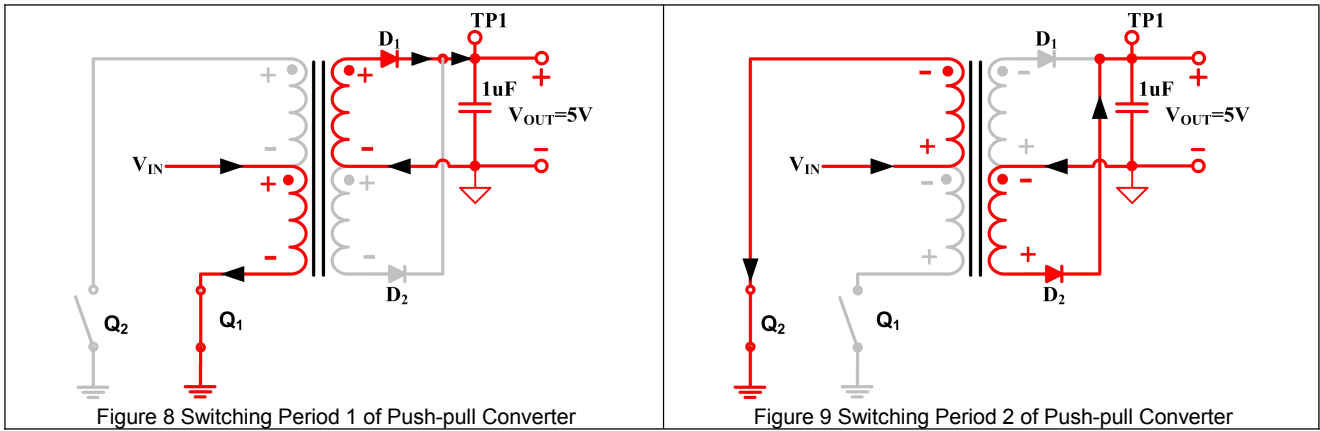


Figure 7 Schematic Diagram of Test Circuit for Switch Characteristics

(1) Push-pull Converter

As shown in Figure 8 and Figure 9, the push-pull converter is a transformer with center tap, which can achieve the transmission of energy from the primary winding to secondary winding.



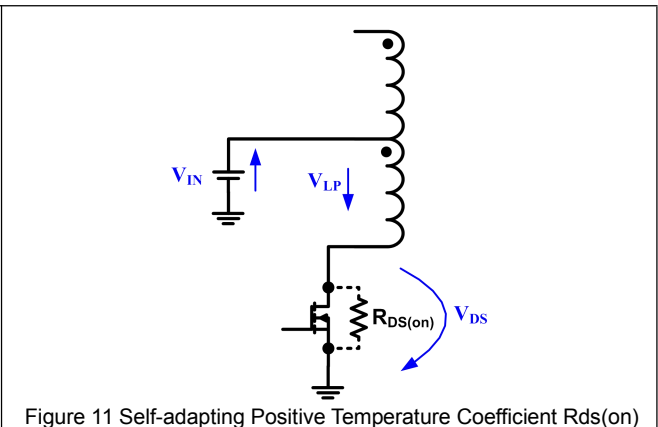
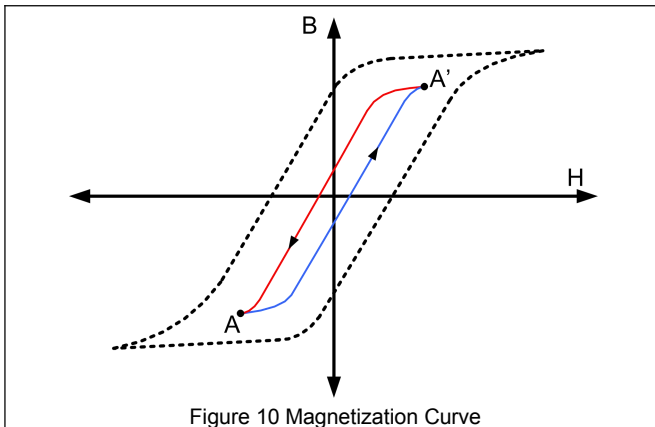
The drive waveform of drains VD1 and VD2 of two MOSFETs Q1 and Q2 are shown in Figure 6. Two MOS transistors are on alternatively and the times of the breakover periods of two transistors are equal, and there is a short period t_{BDM} between the two breakover periods that the two power transistors are not on. That is to say, the drive levels of two MOS transistors are quasi complementary in time sequence, that is the other transistor is off when one transistor is on, but there is a short period of dead time during the switch to prevent the backward current flow when two the transistors are not on simultaneously. As shown in red highlighted parts in Figure 8, when Q1 is on, input voltage V_{IN} drives a current which arrives at the reference ground through the lower half of primary winding of transformer and Q1, and at the same time, the induced electromotive force of side winding charges output capacitor through diode D1, similarly, as shown in Figure 9, when Q2 is on, the induced electromotive force charges output capacitor through diode D2. As continuously repeating the above process, the secondary winding of power converter obtain the needed power supply.

(2) Magnetization of Magnetic Core

Figure 10 is the ideal magnetization curve of push-pull converter, and the vertical axis represents magnetic flux density B and the horizontal axis represents magnetic field intensity H. When Q1 is on, the magnetic flow is pushed to point A' from point A, similarly, when Q2 is on, the magnetic flow is then pulled back to point A from point A'. The magnetic flux density B is proportional to the product of voltage of primary winding V_{LP} and breakover time of MOS transistors t_{ON} , which can be described in the following formula:

$$B \propto V_{LP} \times t_{ON}$$

The volt-second product $V_{LP} \times t_{ON}$ defines the magnetization degree of each switching period. If the volt-second products in the above “push” and “pull” periods are not identical, a small direct current component may be generated to cause the deviation of magnetic flow. If balance cannot be restored, the deviation of magnetic flow will gradually increase in the each of the following switching period, making magnetic core become saturated gradually. The phenomenon of the deviation of magnetic flow is usually caused by the unequal on resistance or switching speed of two power switching components. Although the on resistance or switching speed of the two power components are approximately equal through integrating them into the same wafer with the help of high matching advantage of semiconductor integrated circuit technology, the manufacturing error still exists, causing the small deviation for the breakover time.



Fortunately, the on resistance $R_{DS(on)}$ of MOSFET has positive temperature coefficient, with which SCM1209A has the self-correcting effect to restrain the imbalance of volt-second. Under the condition that there is small deviation between the breakover time of two MOS transistors, the transistor which has longer breakover time t_{ON} generates more quantity of heat, and the temperature of the transistor rises to improve $R_{DS(on)}$, then in the breakover period when the load remains unchanged, the drain-source voltage of this transistor V_{DS} is relatively high, as shown in Figure 11, the voltage of primary winding V_{LP} conforms to the formula $V_{LP} = V_{IN} - V_{DS}$, thus the V_{LP} of the transistor which has larger t_{ON} will gradually decrease to make volt-second recover balance.

SCM1209A has three operation modes, which respectively are start-up mode, operation mode and short mode.

In start-up mode, SCM1209A provides sufficient charging time for output capacitor, to avoid the abnormal start caused by output short circuit which is incorrectly identified due to the excessive low voltage of output capacitor when it is just started; at the same time, the MOS transistor in start-up mode is always operating in current-limiting drive status which means that the drive voltage of MOS transistor in start is limited, thereby making the current flowing through MOS transistor restrained within the safe range of components, that is to restrain the output switching current of primary winding to I_{SOFT} to achieve the soft start of the system, thereby avoiding the over-current impact and the generation of excessive heat.

In operation mode, MOS transistor is always in full drive status which means that the MOS transistor is operating in switching status and the breakover voltage is very low, which guarantee the efficiency of converter.

In short mode, it will stop driving the converter in sleep mode and the heat generated in start-up mode will be dissipated, then the product changes to start-up mode.

The three operation modes can be freely switched. Only when there is abnormality of output short circuit, the product will repeatedly switch between the start-up mode and short mode; when the abnormality disappears, the product will automatically change to operation mode, all of which can fully guarantee the reliability of converter and have no influence on the performance of converter in normal operation.

Start-up Mode

The voltage of output capacitor is zero when the converter is just started, and the converter is firstly in start-up mode. The flow diagram is shown in Figure 12, that is, start → Drive the selected MOS transistor in current-limiting drive method → check the switch-on voltages (V_{VD1} , V_{VD2}) → judge whether the voltages (V_{VD1} , V_{VD2}) are more than the set value.

If (V_{VD1} , V_{VD2}) are more than the set value, then calculate the duration of over-voltage → judge whether the duration is more than T_{D_OSP} (47ms, typ.). If yes, then the system turns into short circuit mode; if no, then the above process is repeated.

If (V_{VD1} , V_{VD2}) are not more than the set value, then the system turns into operation mode.

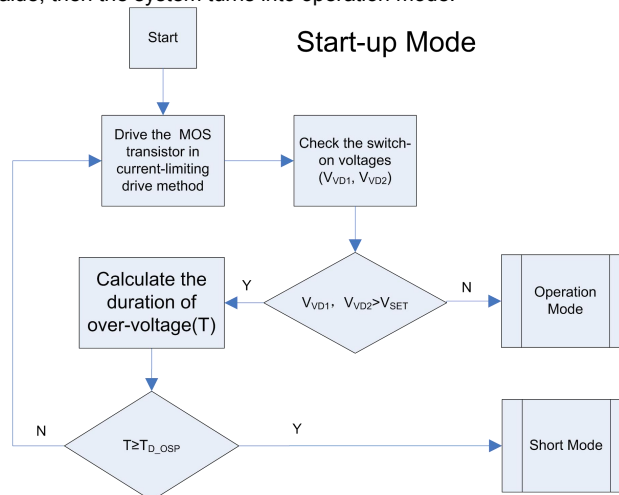


Figure 12 Flow Diagram of Start-up Mode

Operation Mode

If the output of converter has no short circuit, the voltage of output capacitor, in start-up mode, will gradually increase during the continuously circular charging. When the breakover voltage of MOS transistor is less than or equal to the set value, the converter will turn into operation mode. The flow diagram is shown in Figure 13, that is, determine that the breakover voltage of MOS transistor is less than or equal to the set value → drive the selected MOS transistor with full drive → check the switch-on voltage of MOS transistors → judge whether the voltages (V_{VD1} , V_{VD2}) are more than the set value.

If the breakover voltage of MOS transistor is more than the set value, then the system goes into time-counting cycle of start-up mode; otherwise, the system turns back to the step “drive the selected MOS transistor with full drive”, and the above processes are repeated, which is the normal operation of the converter after the product is started. In the operation, MOS transistor is fully driven, that is the MOS transistor is operating in switching status and the on resistance is low, resulting in low energy consumption and high efficiency.

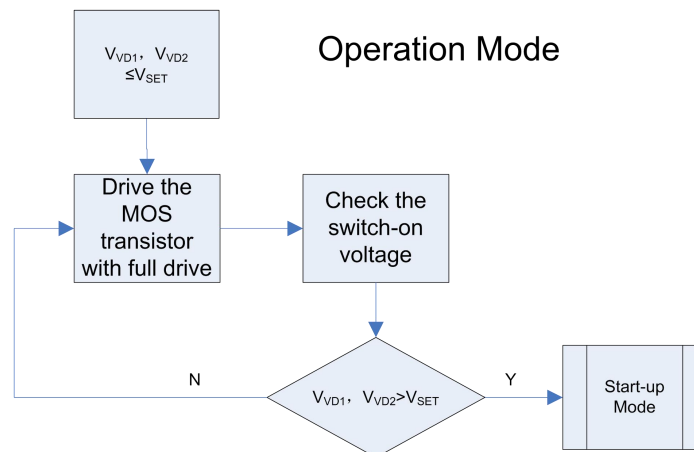


Figure 13 Flow Diagram of Operation Mode

Short Mode

If the output of the converter has short circuit, it will detect in start-up mode that the breakover voltage of MOS transistor is more than the set value, then the accumulated over-voltage time will definitely exceed T_{D_OSP} (47ms,typ.). At this time, SCM1209A will stop to drive the MOS transistor and begin to count the time of stopping driving MOS transistor. When the time is counted to T_{SLEEP} (1s,typ.), the product resumes operation and turns into start-up mode.

The flow diagram of short mode is shown as Figure 14: determine the duration of over-voltage exceeding T_{D_OSP} → stop driving and begin to count time (sleep mode) → finish counting time → turn back to start-up mode. We can see that if the converter is always in output short circuit status, it will operate in the short mode and start-up mode alternately.

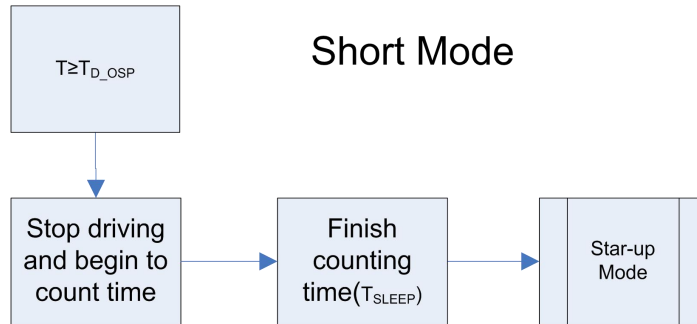


Figure 14 Flow Diagram of Short Mode

Extended Output Design

SCM1209A chip is used to drive the push-pull circuit, which can make output voltage become higher.

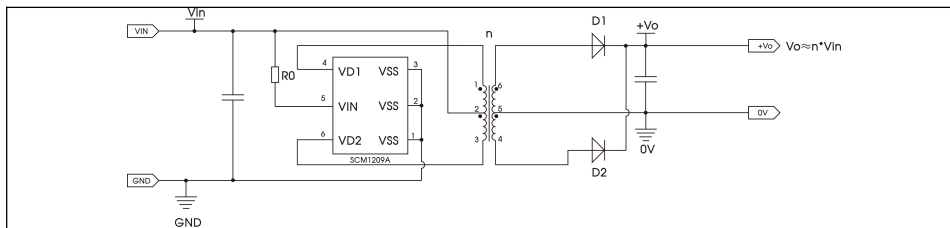


Figure 15 Extended Circuit I

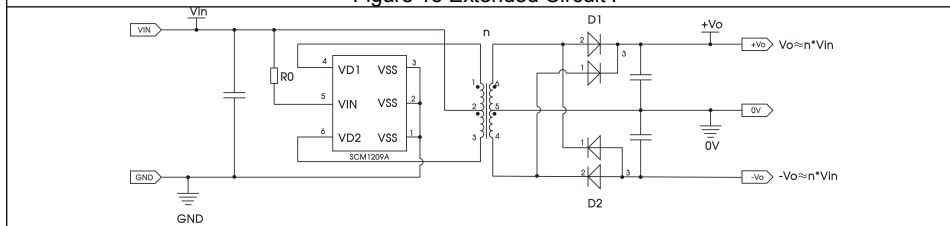


Figure 16 Extended Circuit II

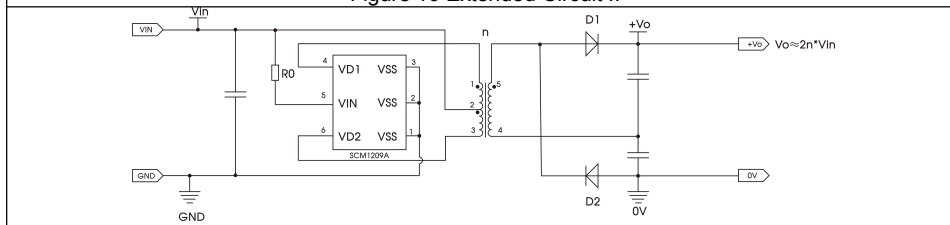


Figure 17 Extended Circuit III

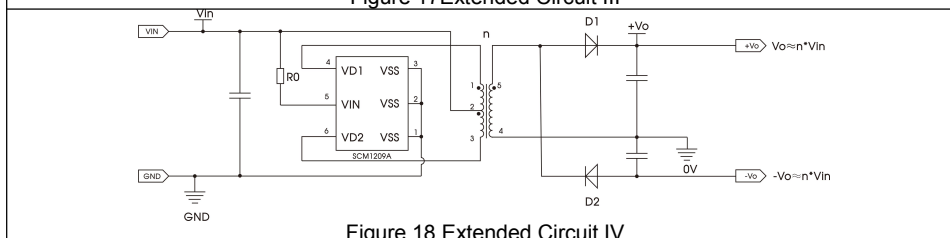
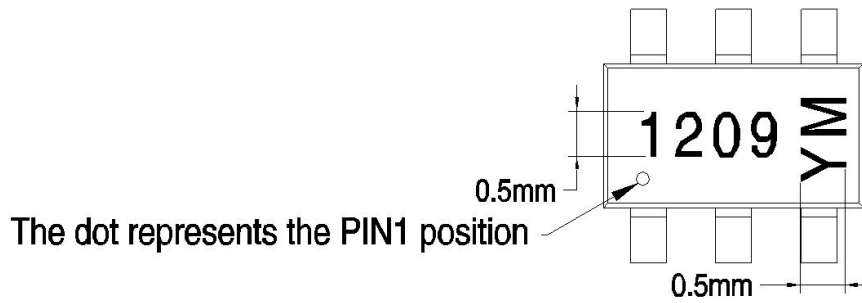
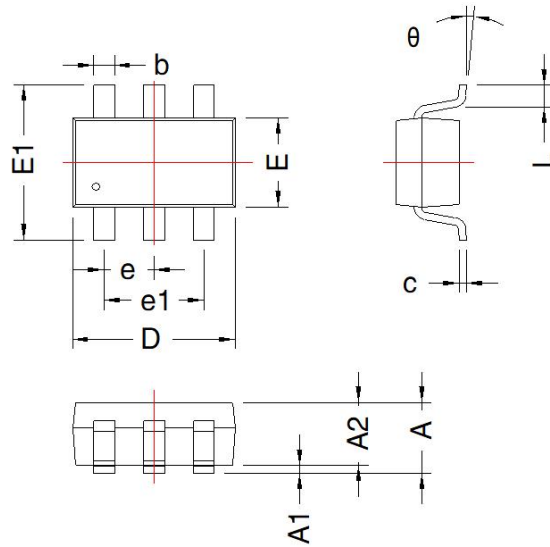


Figure 18 Extended Circuit IV

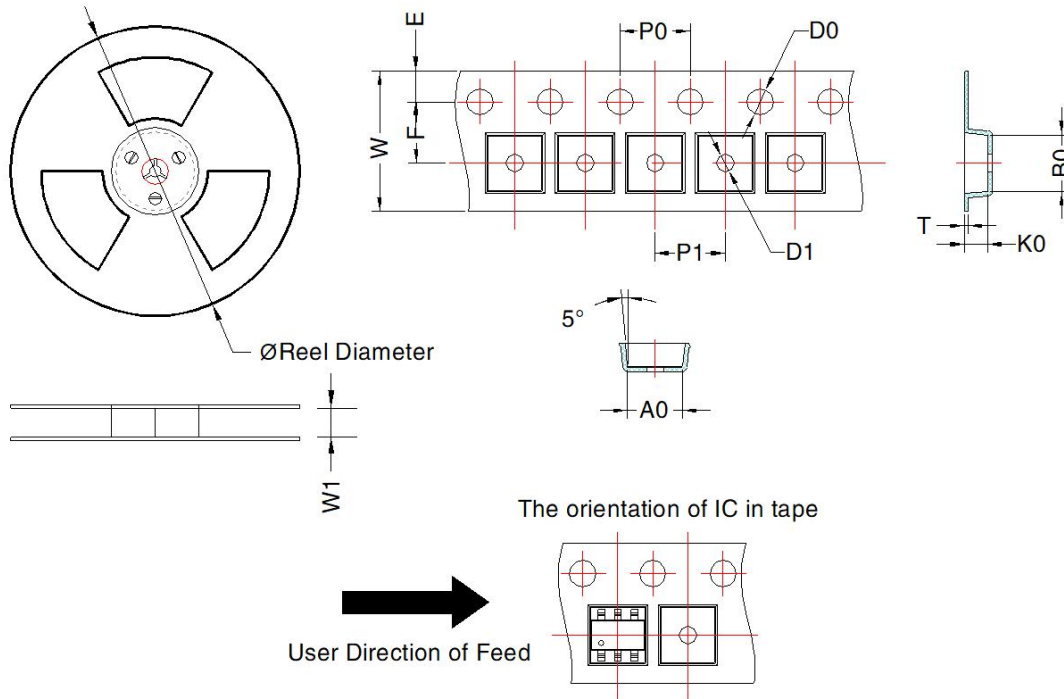


Package Information

THIRD ANGLE PROJECTION



TSOT-23-6				
Mark	Dimension(mm)		Dimension(inch)	
	Min	Max	Min	Max
A	--	1.10	--	0.043
A1	0.00	0.10	0.000	0.004
A2	0.70	1.00	0.028	0.039
D	2.85	2.95	0.112	0.116
E	1.55	1.65	0.061	0.065
E1	2.65	2.95	0.104	0.116
L	0.30	0.60	0.012	0.024
b	0.30	0.50	0.012	0.020
e	0.95 TYP		0.037 TYP	
e1	1.90 TYP		0.075 TYP	
c	0.08	0.20	0.003	0.008
θ	0°	8°	0°	8°



Device	Package Type	MPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	T (mm)	W (mm)	E (mm)	F (mm)	P1 (mm)	P0 (mm)	D0 (mm)	D1 (mm)
SCM1209ATA	TSOT-23-6	3000	180.0	8.5	3.17 ± 0.1	3.1 ± 0.1	1.1 ± 0.1	0.25 ± 0.03	8.0 ± 0.3	1.75 ± 0.1	3.5 ± 0.1	4 ± 0.1	4 ± 0.1	1.5 ± 0.1	1.0 ± 0.1

Note: The minimum order quantity is the minimum packing quantity, and the order quantity shall be an integral multiple of MPQ.

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